

A fictitious domain method on Octrees/Basilisk

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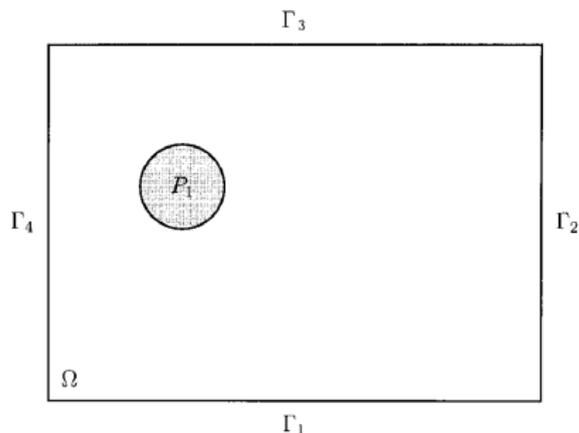


Particle laden flow with basilisk



Fictitious domain method: principle

Consider a domain Ω with boundaries $\Gamma_1, \dots, \Gamma_4$ filled with (Newtonian) fluid and an (homogeneous) solid particle occupying the domain $P(t)$ with boundary $\partial P(t)$:



fluid domain: $\Omega \setminus \overline{P(t)}$

solid domain: $P(t)$ with
boundary $\partial P(t)$

Reference: (Glowinski et al., 1999).



Fictitious domain method: starting point (in strong form)

- combined-equations of motion with Lagrange multipliers λ :

$$\rho_L \left(\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} \right) = -\nabla p + \nabla \cdot (2\mu \mathbf{D}) - \lambda \text{ in } \Omega,$$

$$\left(1 - \frac{\rho_L}{\rho_s} \right) \left(M \left(\frac{d\mathbf{U}}{dt} - \mathbf{g} \right) \right) = \int_{P(t)} \lambda \, d\mathbf{x} \text{ in } P(t),$$

$$\left(1 - \frac{\rho_L}{\rho_s} \right) \left(\mathbf{I} \frac{d\boldsymbol{\omega}}{dt} + \boldsymbol{\omega} \times \mathbf{I} \boldsymbol{\omega} \right) = \int_{P(t)} \mathbf{r} \times \lambda \, d\mathbf{x} \text{ in } P(t)$$

$$\mathbf{u} - (\mathbf{U} + \boldsymbol{\omega} \times \mathbf{r}) = 0 \text{ over } P(t)$$

- continuity equation

$$-\nabla \cdot \mathbf{u} = 0 \text{ over } \Omega$$

- unknowns: $\mathbf{u}, p, \mathbf{U}, \boldsymbol{\omega}, \lambda$



Operator splitting

The process can be seen as a particular initial value problem:

$$\frac{d\phi}{dt} + \mathbf{NS}(\phi) + \mathbf{Gra}(\phi) + \mathbf{Fd}(\phi) = f$$
$$\phi(t=0) = \phi_0.$$

Split in 3 and solve successively (Glowinski et al., 1999):

$$\frac{\phi^{n+1/3} - \phi^n}{\Delta t} + \mathbf{NS}(\phi^{n+1/3}) = f_1^{n+1},$$
$$\frac{\phi^{n+2/3} - \phi^{n+1/3}}{\Delta t} + \mathbf{Gra}(\phi^{n+2/3}) = f_2^{n+1},$$
$$\frac{\phi^{n+1} - \phi^{n+2/3}}{\Delta t} + \mathbf{Fd}(\phi^{n+1}) = f_3^{n+1},$$

with $f_1^{n+1} + f_2^{n+1} + f_3^{n+1} = f((n+1)\Delta t)$.



Operator splitting

Pros:

- Flexible for the choice of each sub-problem's solvers: use any available solver in your group/internet.
- Relatively easy to implement
- Robust (stable) and preserves stationary solutions (MacNamara and Strang, 2016)

Cons:

- First order accurate only



Validation: Stokes flow through a periodic array of spheres

Tri-periodic domain. Flow initially at rest, motion imposed with a pressure gradient.

Drag coefficient K , D diameter, ϕ concentration, V superficial velocity

$$F_i = 3\pi\mu DKV_i$$

$$D/2 = (3\phi/4\pi)^{1/3}$$

$$V_i = \frac{1}{\tau_0} \iiint_{\Omega/P} u_i(\mathbf{x}) d\mathbf{x}$$

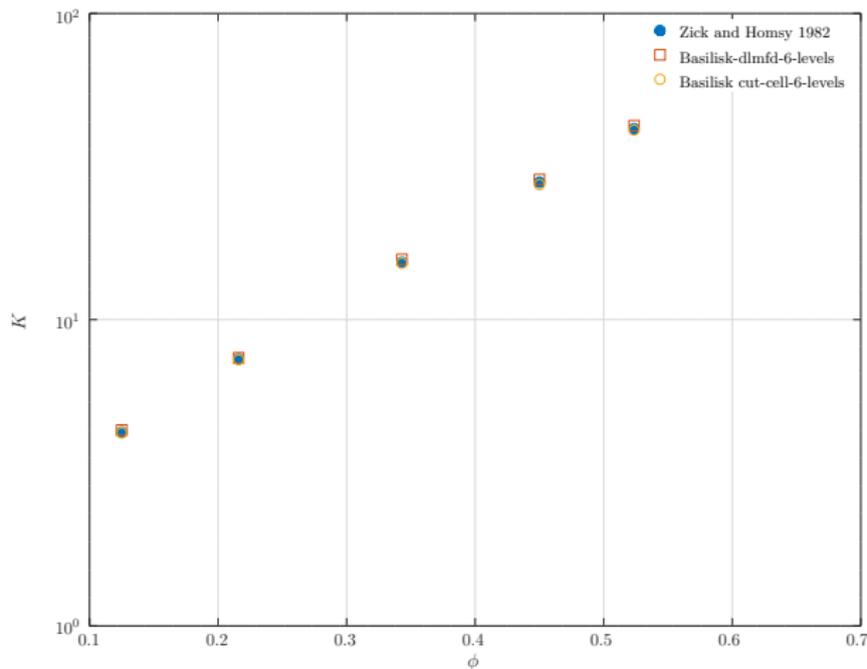
Zick and Homsy (1982)

streamwise velocity



Validation: Stokes flow through a periodic array of spheres

Validation of octrees with constant 2^6 cells per direction.

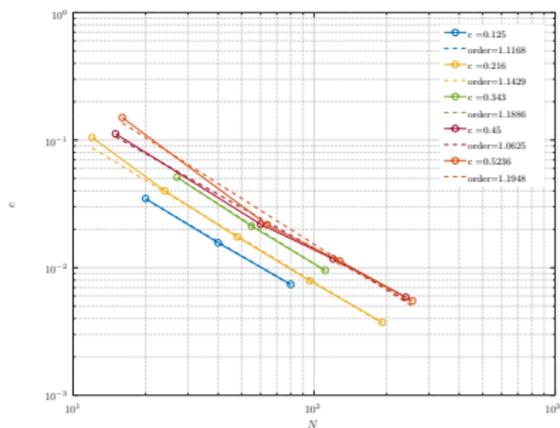


Drag coefficient K as a function of the concentration ϕ .

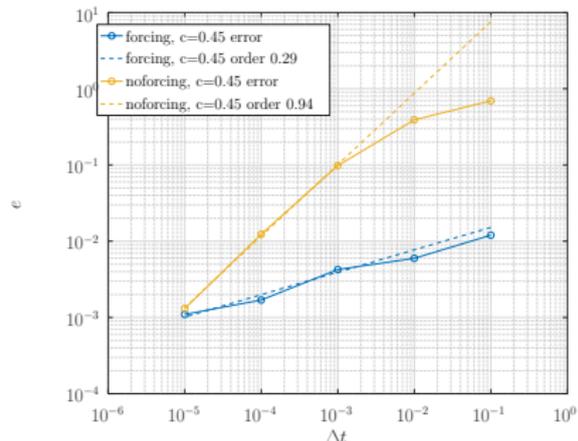


Validation: Stokes flow through a periodic array of spheres

First order convergence rate in space and time.



Spatial convergence

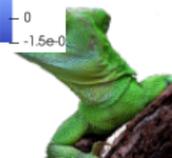
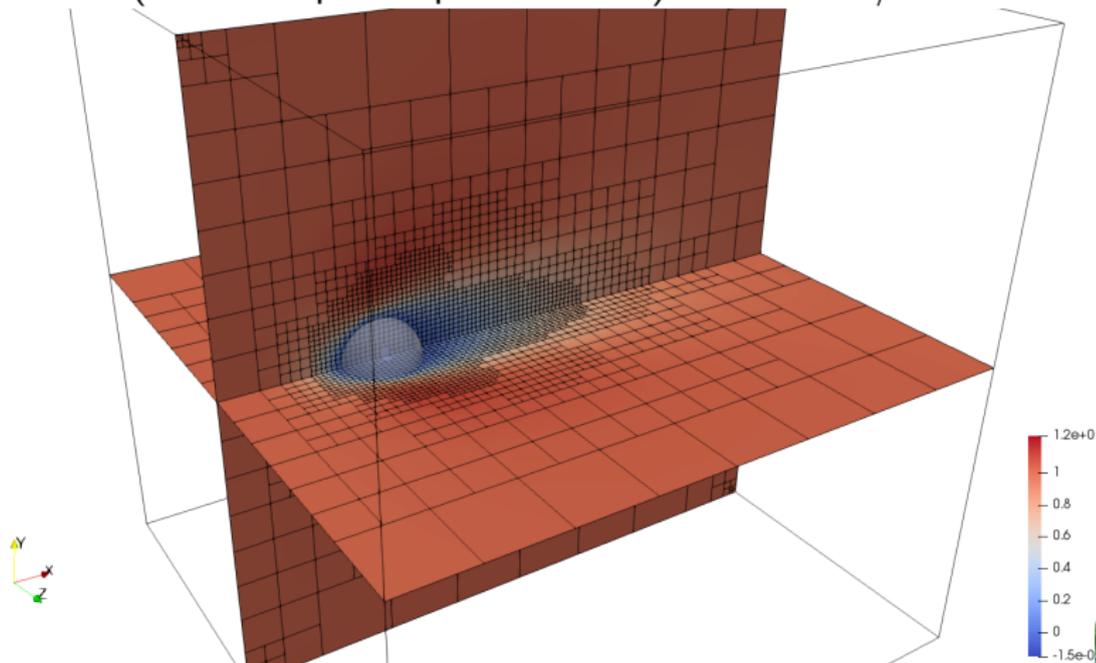


Temporal convergence



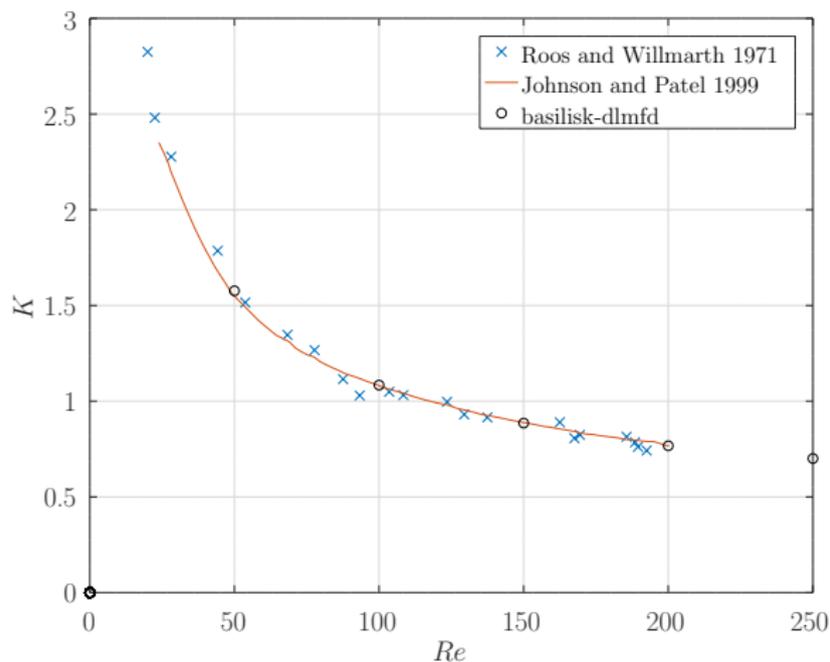
Validation: Flow past a sphere, adaptive meshes

Flow past a sphere at $50 \leq Re \leq 250$ with $N = 9, \dots, 13$ level of refinement (34 – 136 points per diameter). Box size $L/D = 30$.



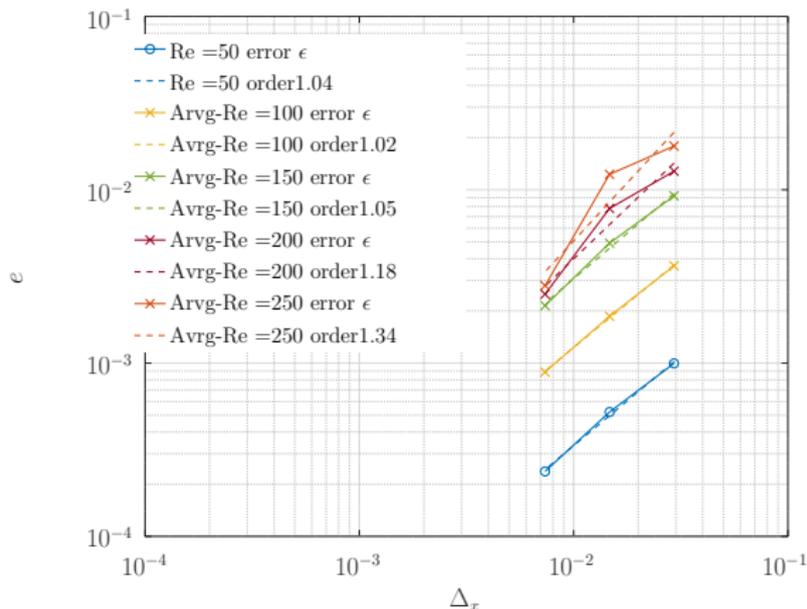
Validation: Flow past a sphere, adaptive meshes

Comparison of the drag coefficient $K(Re)$ against previous works.



Validation: Flow past a sphere, adaptive meshes

Spatial convergence rate: ranging from 1.04 to 1.34.



Validation: flow past a cylinder at $Re = 9500$

15 level of refinement, domain size $L/D = 18$, resolution $2^{15}/18 \sim 1820 \text{pts}/D$. Equivalent cartesian grid $2^{30} \sim 10^9$ cells

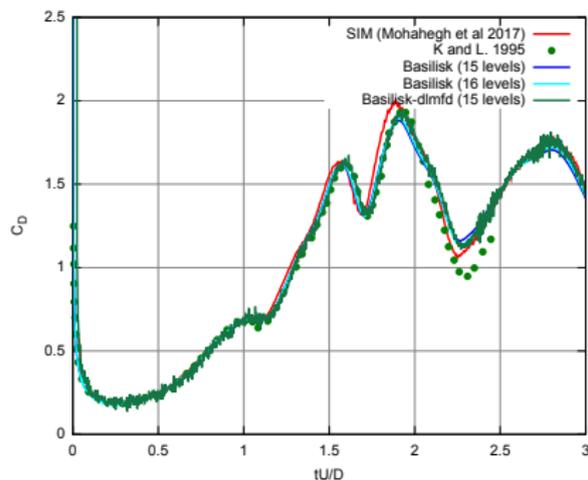
Axial vorticity $\omega_z(t)$

Animation of the mesh

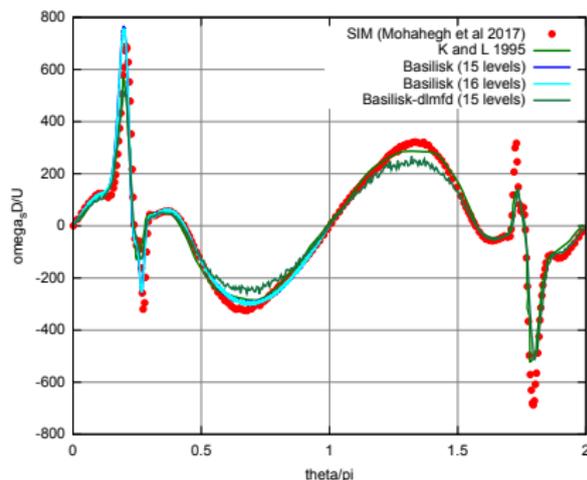


Validation: flow past a cylinder at $Re = 9500$

Comparison with respect to other codes/papers/techniques:



Drag coefficient C_D

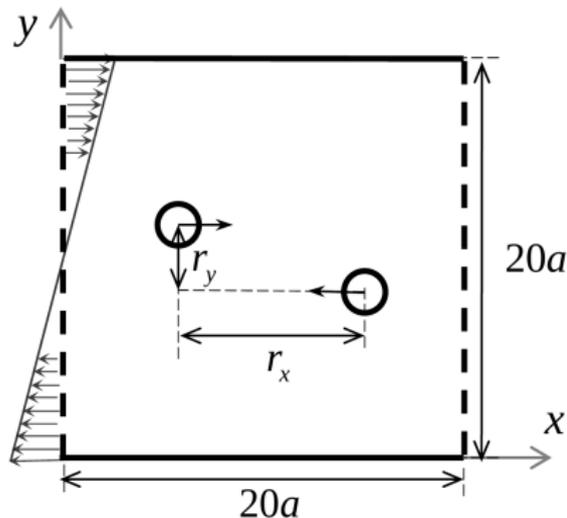


Surface vorticity at $t = 2.5$

More at <http://basilisk.fr/sandbox/cselcuk/starting-dlmfd.c>



Two moving spheres in creeping shear flow



\vec{r} : inter-particle distance

a : sphere's radius

"Analytical" solution:

$$\frac{dr_x}{dt} = r_y + er_x - \frac{B(\vec{r})}{2} r_y,$$

$$\frac{dr_y}{dt} = er_y - \frac{B(\vec{r})}{2} r_x,$$

$$\frac{dr_z}{dt} = er_z,$$

where

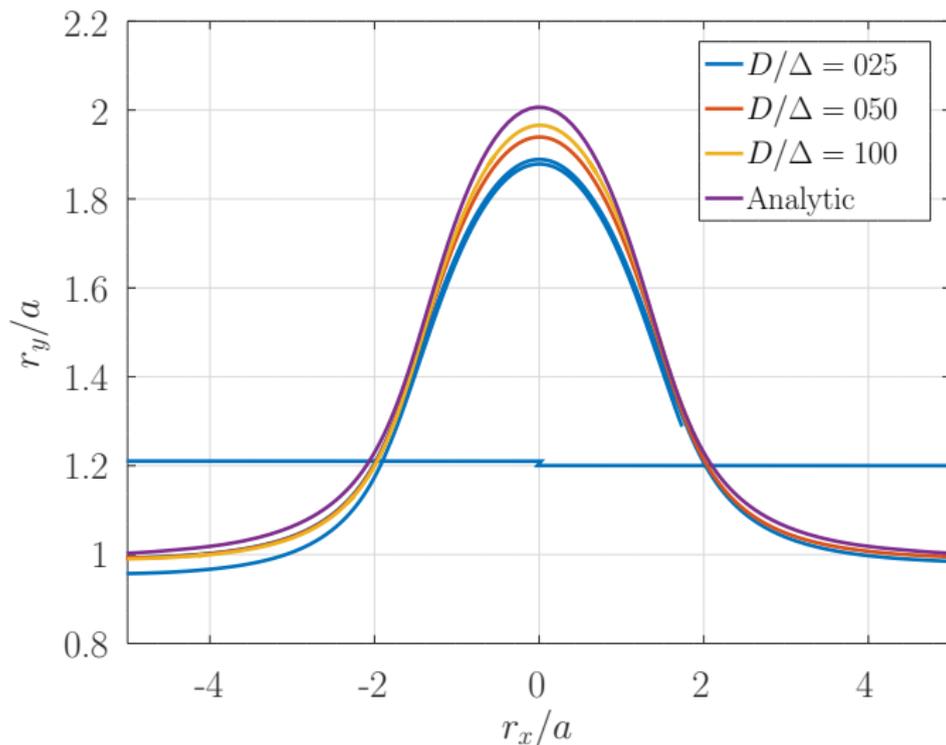
$$e = \frac{r_x r_y (B(\vec{r}) - A(\vec{r}))}{\vec{r}^2},$$

(Batchelor and Green, 1972) and (Lin et al., 1970)



Two moving spheres in creeping shear flow

Time-step $\Delta t = 1/3000$:



Two moving cylinders in creeping shear flow

2D: Time-step $\Delta t = 1/3000$, mesh size $D/\Delta \sim 200$, 11 levels of refinement

refinement criterion on \vec{u} and the color field

refinement criterion only on the color field



Attempt to capture lubrication forces: preliminary conclusion

Globally encouraging results:

- Lubrication force almost fully captured by brute-forcing
- No contact and sub-grid models
- Robust even when particles overlap



Dynamic of multiple particles with Grains 3D

Coupling with Grains3D as granular solver (C++ code) with Basilisk's Navier-Stokes solver (C code).



Dynamic of a free falling cube, $\rho_s/\rho_s = 7$, $Ga = 140$

Box size $L/D = 700$, (equivalent) spatial resolution $\sim 25pts/D$.



Dynamic of cluster of (600) particles at $Re = 15$

Simulations performed by Daniel Oliveira (L.S.U)

Basilisk dlmfd + grain3D

Experiments by (Pignatel et al.,
2011)



Thank you

Thank you for your attention !

More on my sandbox at: <http://basilisk.fr/sandbox/cselcuk/>



The first, Navier-Stokes problem

Basilisk's global temporal-scheme for the Navier-Stokes problem reads: given \mathbf{u}^n, λ^n , find $\mathbf{u}^{n+1/2}, p^{n+1/2}$ such that:

$$\frac{\mathbf{u}^{n+1/2} - \mathbf{u}^n}{\Delta t} = - [\mathbf{u} \cdot \nabla \mathbf{u}]^{n+1/4} + \frac{1}{\rho_f} \left[\nabla \cdot \left(2\mu \mathcal{D}_v^{n+1/2} [\mathbf{u}^{n+1/2}] \right) - \nabla p^{n+1/2} \right] - \lambda^n,$$
$$\nabla \cdot \mathbf{u}^{n+1/2} = 0.$$

Solved with a modified version of the projection scheme proposed by (Bell et al., 1989).



The second, granular problem

The second sub-problem is a pure granular problem which reads:
given $\mathbf{U}_i^n, \boldsymbol{\omega}_i^n$ find $\mathbf{U}_i^{n+1/2}, \boldsymbol{\omega}_i^{n+1/2}$ such that

$$\left(1 - \frac{\rho_f}{\rho_s}\right) M \left(\frac{\mathbf{U}^{n+1/2} - \mathbf{U}^n}{\Delta t}\right) = \left(1 - \frac{\rho_f}{\rho_s}\right) M \mathbf{g} + \mathbf{F} \mathbf{c}$$
$$\left(1 - \frac{\rho_f}{\rho_s}\right) \mathbf{I} \left(\frac{\boldsymbol{\omega}^{n+1/2} - \boldsymbol{\omega}^n}{\Delta t}\right) = - \left(1 - \frac{\rho_f}{\rho_s}\right) \boldsymbol{\omega}^n \times \mathbf{I} \boldsymbol{\omega}^n + \mathbf{T} \mathbf{c}.$$

Can be solved with any granular solver that handles contact forces and torques for multiple particles.



The third, fictitious-domain problem

The fictitious-domain problem reads: given $\mathbf{u}^{n+1/2}$, λ^n , $\mathbf{U}^{n+1/2}$, $\boldsymbol{\omega}^{n+1/2}$ solve

$$\rho_f \left(\frac{\mathbf{u}^{n+1} - \mathbf{u}^{n+1/2}}{\Delta t} \right) - \lambda^{n+1} = \lambda^n \text{ over } \Omega$$

$$\left(1 - \frac{\rho_f}{\rho_s} \right) \left(M \left[\frac{\mathbf{U}^{n+1} - \mathbf{U}^{n+1/2}}{\Delta t} \right] \right) = - \int_{P(t)} \lambda^{n+1} \, d\mathbf{x} \text{ over } P(t)$$

$$\left(1 - \frac{\rho_f}{\rho_s} \right) \left(\mathbf{I} \left(\frac{\boldsymbol{\omega}^{n+1} - \boldsymbol{\omega}^{n+1/2}}{\Delta t} \right) \right) = - \int_{P(t)} \mathbf{r} \times \lambda^{n+1} \, d\mathbf{x} \text{ over } P(t)$$

$$\mathbf{u}^{n+1} - \left(\mathbf{U}^{n+1} + \boldsymbol{\omega}^{n+1} \times \mathbf{r} \right) = \mathbf{0} \text{ over } P(t).$$

Saddle-point problem solved with an iterative algorithm (Uwaza).

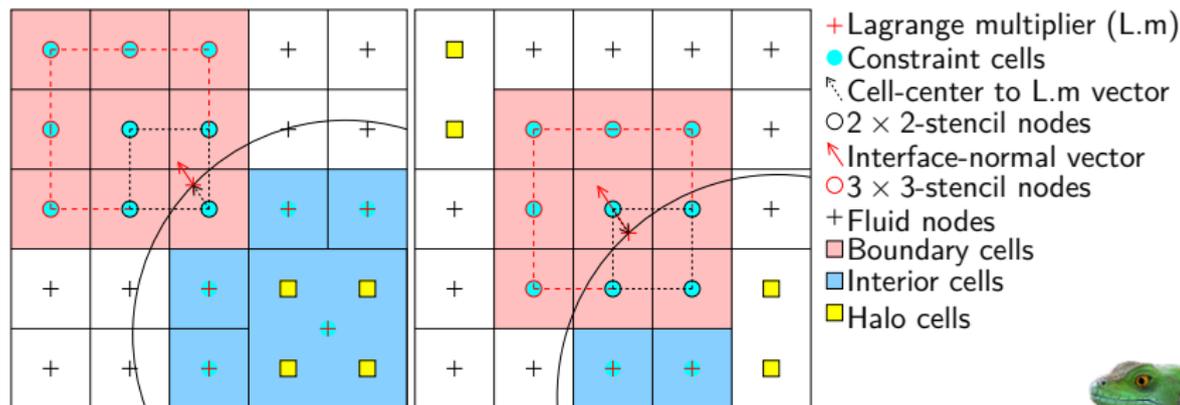


Interface reconstruction

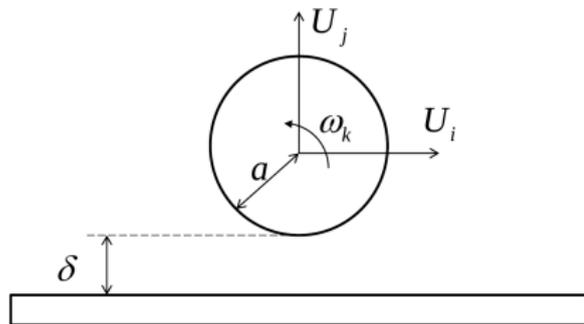
Collocation point method: use of a Dirac delta function as basis function for the Lagrange multipliers λ :

$$\lambda(\mathbf{x}) = \sum_{l=1}^L \lambda_l \delta(\mathbf{x} - \mathbf{x}_l). \quad (1)$$

with L the number of Lagrange multipliers.



One sphere close to wall in Stokes flow



δ : gap distance
 a : sphere's radius

- Large box: $L/a = 60$
- Periodicity on front/back and left/right faces
- "Wall" for bottom/top faces
- fixed particle
- imposed velocity:
 $\vec{U} = (0, -U_c, 0)$, $\vec{\omega} = \vec{0}$
- $T_c = 2a/U_c$

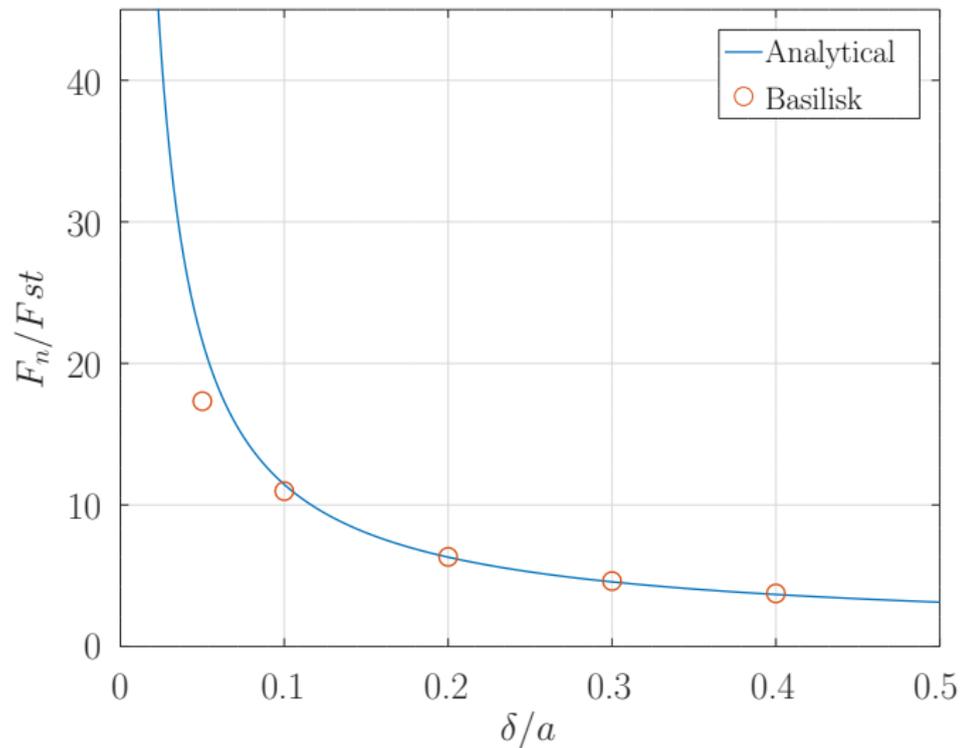
Analytical solution:

$$F_n/F_{st} = (\delta/a)^{-1} - \frac{1}{5} \log(\delta/a) + 0.97128, \quad (2)$$

(Brenner, 1961) and (Cooley and O'Neill, 1969)



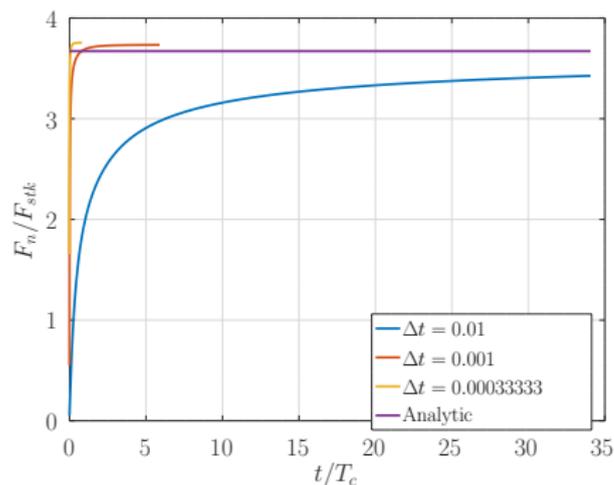
One sphere close to wall in Stokes flow



One sphere close to wall: temporal convergence

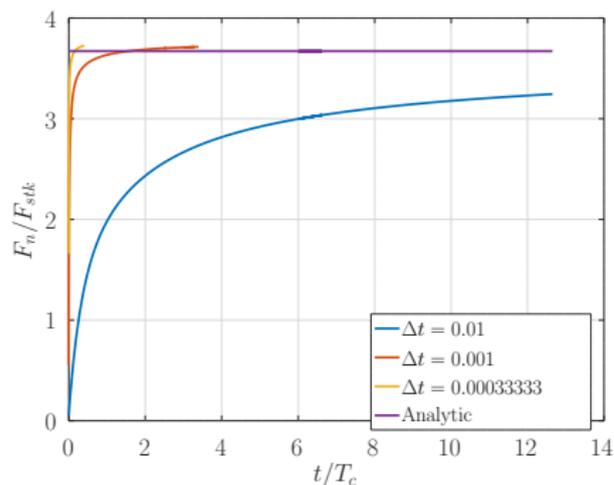
case: $\delta/a = 0.4$:

$a/\Delta \sim 34$, $\delta/\Delta \sim 25$



11 levels of refinement

$a/\Delta \sim 68$, $\delta/\Delta \sim 50$



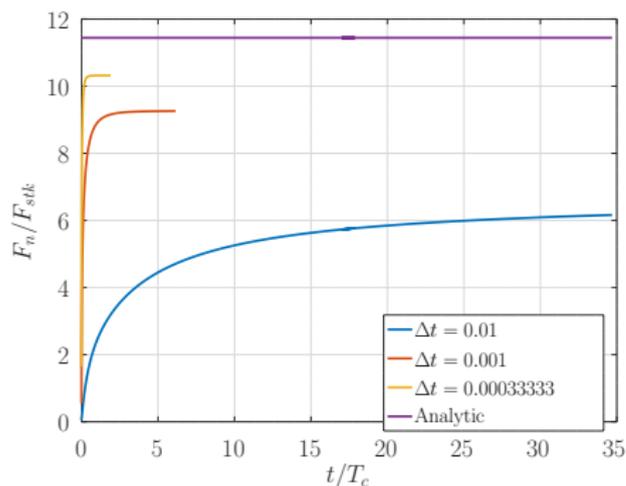
12 levels of refinement



One sphere close to wall: temporal convergence

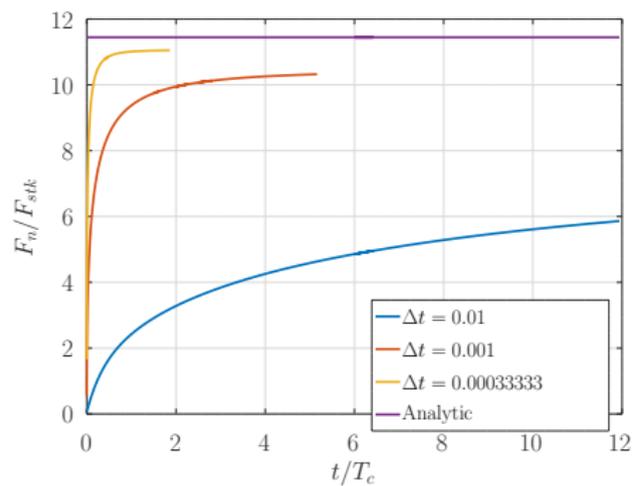
More challenging case: $\delta/a = 0.1$:

$a/\Delta \sim 34$, $\delta/\Delta \sim 3$



11 levels of refinement

$a/\Delta \sim 68$, $\delta/\Delta \sim 6$



12 levels of refinement

