MODELLING OF LIQUID STEEL, SLAG IN AN ARGON GAS BOTTOM BLOWN REACTOR

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Overall description of a steel mill



Slag :

by-product of metal contain metal oxides and silicon dioxide 2700kg/m³,7.10⁻²Pa.s, 1,2 N/m

Secondary metallurgy: Liquid steel at 1600°C treated in 200 ton ladle 7000kg/m³; 5.10⁻³Pa.s, 1,5 N/m • Refinement of liquid steel:

- Desulfurization of liquid steel by chemical reaction with slag:

 $[S] + (CaO) \leftrightarrow (CaS) + [O]$

- Ladle is stirred with Argon bubbling to produce:
- renewal of steel in contact with slag



Summary

- I- Simulation and experiment of the process
- II- Comparison of numerical and experimental results
- III- Conclusion

Use a scale model based on the work of S.H. *Kim et al.* 1987

Froude similarity between scale and industrial ladle

$$\begin{split} \lambda_{1} &= \frac{d_{0Kim}}{d_{0model}} = 2,2; \ \lambda_{2} = \frac{d_{0industrial}}{d_{0mode}} = 16,6 \\ N'_{Fr} &= \frac{\left(\rho_{g}u_{0}\right)^{2}}{\rho_{l}\rho_{g}gL} \\ N'_{Fr} &= C \frac{\dot{Q}g^{2}}{Ld_{0}^{4}} \\ \dot{Q}_{Kim} &= (\lambda)^{\frac{5}{2}} \dot{Q}_{model} \\ \dot{Q}_{industrial} &= 1,038(\lambda)^{\frac{5}{2}} \dot{Q}_{model} \end{split}$$

Process - model

Three phases air, water, oil at 20°C

- oil \rightarrow slag
- water \rightarrow liquid steel
- air \rightarrow argon gas

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$$M = \frac{g\mu_l^4 \Delta \rho}{\rho_l^2 \sigma_{g/l^3}}$$
; $Bo = \frac{\Delta \rho g d^2}{\sigma_{g/l}}$

- $D_{b,industrial} = 12cm$
- $M_{industrial} = 2.6E 13$
- $Eo_{industrial} = Bo = 715$
- $D_{b,model} = 8.2mm$
- $M_{model} = 2.65E 11$
- $Eo_{model} = Bo = 9$





<u>http://basilisk.fr/sandbox/joubert/three-phase.h</u>

Add a third phase explicitly.

http://basilisk.fr/sandbox/joubert/conserving3f.h

Modify the function to have momentum conservation for three explicit phase.

Process simulation - setup

We set for numerical reasons $\rho'_a = 10\rho_a = 12,25\frac{kg}{m_3}$

Oka & Ishii (1998), Tryggvason, Cano-Lozano (2016)

- Water/air density ratio R=82
 Water/air viscosity ratio M=54
- $\rho(\chi) \equiv f_1 \rho_1 + f_2 \rho_2 + f_3 \rho_3$
- $\mu(\chi) \equiv f_1 \mu_1 + f_2 \mu_2 + f_3 \mu_3$
- $\sigma_{12} = \sigma_1 + \sigma_2$

K.A Smith et al. 2002 X. Chen et al. 2017 (Gerris)

$$\chi_{kn}(x,t) = \frac{\chi_k(x,t)}{\sum_i^n \chi_k(x,t)}$$

Process -experimental results – visualisation



/04/2019 14:47:04 -11220,3[ms] 000000000 EoSens Cube6 [00-11-1c-f1-73-3a] Mikrotron 1280x1024 50fps 1800µs

Face view of hydraulic model, zoom at interface at Qg=5,0L/min with Dinj=2,35mm

Process simulation- numbers



This work was granted access to the HPC resources of CINES under the allocation 2018- A0052B07760 *made by GENCI*

=264*µm*

Process simulation – Results

Front view model: with fast camera



Front view simulation: oil interface in red, air in green



Process simulation – Results

Topview model with camera;



Topview oil phase in red



Process simulation – Results

Evolution of kinetic energy with time



Process experimental visualisation - Open eye



Comparison of numerical and experimental – Results



For now manual post-processing with 4 frames per gas flow rate

Comparison of numerical and experimental – Results

Open eye area comparison with literature and simulation:



Conclusion

- Establish a simple workable three phase model with three surface tension values.
- Results comparison from simulations and from image analysis of the experiments gives reasonable agreement.
- Evaluate mass transfer of a chemical species between water and oil through different method.

Questions

9.500e-01 8.500e-01 7.500e-01 6.500e-01 5.500e-01 4.500e-01 3.500e-01 2.500e-01 1.500e-01 5.000e-02

